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EXPLOSIVE ACCELERATION OF PROJECTILES

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$$\rho = 8\rho_0(x/t + D/2)/9D$$
 (2c)

Since Region I is a simple wave mapped on ab of Figure 2, any curve traversing Region I lies on ab. In particular the line PG, which separates Region II from Region I, lies on ab. PG is the leading C- characteristic of the fan passing through P of Figure 1, so

$$(dx/dt)_{PG} = u - c = (x - a)/(t - a/D)$$

But, since PG maps onto ab of Figure 2, u - c = -D/2 and

$$(x - a)/(t - a/D) = -D/2$$

PG is then parallel to OF, and for every other C- characteristic passing through P,

$$dx/dt = (x - a)/(t - a/D) > -D/2$$

For Region II:

C-:
$$u - c = (x - a)/(t - a/D)$$

C+: $u + c = x/t$
 $u = [x/t + (x - a)/(t - a/D)]/2$ (3a)

$$c = [x/t - (x - a)/(t - a/D)]/2$$
 (3b)

$$\rho = 16\rho_0 c/9D \tag{3c}$$

Region II of Figure 1 maps into the triangle abf of Figure 2.

B. Case E2

The explosive is bounded at x = 0 by a rigid backing and at x = a by a void. The flow field is shown in Figure 3. Region I behind the detonation front is a simple wave centered at (0, 0). Reflection at the free surface produces a backward-facing wave centered at A. The interaction of this wave with the Taylor wave and the rigid boundary produces the distinct and identifiable regions shown. Region III is a uniform state bounded by the last characteristic of the Taylor wave, OH, the leading characteristic of the reflection fan, AC, and the rigid boundary. The necessity for such a uniform region is shown in Figure 4. Here the point "a" is the Chapman-Jouget



Region I in the (x, t) plane is bounded by the detonation front OP, by the C+ characteristic OF, and by the C- characteristic PG. The Chapman-Jouget state along OP is represented by point "a" in Figure 2, and the forward-facing rarefaction of Region I lies on the Γ - curve ab. Point b in Figure 2 is the image of OF in Figure 1, which consequently has a slope dt/dx = -2/D.

Reflection of the detonation wave from the free surface at x = a (Figure 1) produces a rarefaction fan with straight C- characteristics centered at the point P(x = a, t = a/D). The detonation gases are then accelerated into the void (x > a) with limiting velocity D. Forward expansion is along af in Figure 2, and a region of overlap between the reflected rarefaction and the rarefaction following the detonation (the Taylor wave) is established as Region II of Figure 1.

For Region I:

C+:
$$u + c = x/t$$

C-: $u - c = -D/2$
 $u = (x/t - D/2)/2$ (2a)



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Figure 3 Flon field for confined explosive, case E2.



Figure 4 Hodograph mapping of flow field E1 of Figure 3.

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Israel J. Techn., state, and Region I lies along the Γ -characteristic ab. Region I terminates at u = 0, the condition imposed by the rigid boundary. Region III of Figure 3 is then mapped into the single point "III" of Figure 4. A traverse around the point A from OA to AB lies on or very close to the Γ + characteristic ac in Figure 4. Region II of Figure 3 is mapped into the quadrilateral acdr of Figure 4. The boundary characteristic, OH, lies along dr. Region IV is again a simple wave region mapped onto the Γ + characteristic u + c = D/2, shown in Figure 4. Region V is a mixed region resulting from interaction of the reflected rarefaction centered at A with its image in the x = 0 plane. The t-axis from C upward maps into the u = 0 axis, Or in Figure IV. The boundary CG corresponds to dr in Figure 4, and the open side of the triangular region V maps into Od of Figure 4. In symbols, these relations can be expressed as follows:

Region	I:	Same as	Region	I of Case E1.	
Region	п:	Same as	Region	II of Case E1.	
Region	III:				

u = 0	(4a)

$$c = D/2 \tag{4b}$$

$$\rho = 8\rho_0/9 \tag{4c}$$

Region IV:

$\mathbf{C}+: u+c=D/2$	
C-: $u - c = (x - a)/(t - a/D)$	
u = [D/2 + (x - a)/(t - a/D)]/2	(5a)
c = [D/2 - (x - a)/(t - a/D)]/2	(5b)
$a = 16\rho_0 c/9D$	(5c)

Region V:

C+:
$$u + c = (x + a)/(t - a/D)$$

C-:
$$u - c = (x - a)/(t - a/D)$$

$$u = x/(t - a/D) \tag{6a}$$

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$$c = a/(t - a/D) \tag{6b}$$

$$\rho = 16\rho_0 a/9D(t - a/D)$$
 (6c)